2. (Previously Presented) Crystal oriented ceramics according to claim 1 wherein, the specific crystal plane is the pseudo-cubic {100} plane and its degree of orientation as determined according to the Lotgering method is 30% or more.

3. (Original) Crystal oriented ceramics according to claim 1 wherein, the piezoelectric d_{31} constant at room temperature is 1.1 times or more that of a non-oriented sintered compact having the same composition.

4. (Original) Crystal oriented ceramics according to claim 1 wherein, the electromechanical coupling coefficient k_p at room temperature is 1.1 times or more that of a non-oriented sintered compact having the same composition.

5. (Original) Crystal oriented ceramics according to claim 1 wherein, the piezoelectric g_{31} constant at room temperature is 1.1 times or more that of a non-oriented sintered compact having the same composition.

6. (Original) Crystal oriented ceramics according to claim 1 wherein, the rate of improvement resulting from orientation in displacement generated under electric field driving conditions having a constant amplitude of an electric field strength of 100 V/mm or more at a predetermined temperature equal to or below the Curie temperature is 1.1 times.

7. (Original) Crystal oriented ceramics according to claim 1 wherein, there is a temperature range where the amount of fluctuation of displacement under electric field driving conditions having a constant amplitude of an electric field strength of 100 V/mm or more over an arbitrary temperature range of 100°C or more equal to or lower than the Curie temperature is within ±20%.

8. Cancelled.

9. (Original) Crystal oriented ceramics according to claim 1 wherein, there is a temperature range where the amount of fluctuation of the value defined by $D_{33large}/(E_{33large})^{1/2}$ under electric field driving conditions having a constant amplitude over an arbitrary temperature range of 100°C or more equal to or lower than the Curie temperature is within ±10%; wherein, D33large is the displacement generated in a direction parallel to the direction in which voltage is applied in the case of applying a high voltage, and is defined by equation A2:

$$D_{33large} = S_{max}/EF_{max} = (\Delta L/L)/(V/L) \qquad \text{A2}$$

(wherein, S_{max} represents the maximum strain, ΔL represents the displacement induced by the electric field (m), L represents the original length prior to applying a voltage (m), and V represents the applied voltage (V)).

10. (Previously Presented) Crystal oriented ceramics according to claim 1 wherein, there is a temperature range where the amount of fluctuation of the value defined by $D_{33large}/E_{33large}$ under electric field driving conditions having a constant amplitude over an arbitrary temperature range of 100°C or more equal to or lower than the Curie temperature is within ±8%.

11. (Original) Crystal oriented ceramics according to claim 1 wherein, there is a temperature range where the amount of fluctuation of displacement generated under constant energy driving conditions over an arbitrary temperature range of 100°C or more equal to or lower than the Curie Temperature is within ±10%.

12. (Previously Presented) Crystal oriented ceramics according to claim 1 wherein, there is a temperature range where the amount of fluctuation of displacement generated under

constant charge driving conditions over an arbitrary temperature range of 100°C or more equal to or lower than the Curie temperature is within ±8%.

13. (Previously Presented) Crystal oriented ceramics according to claim 1 wherein, a crystal system of said crystal grain is a tetragonal system over an arbitrary temperature range of 100°C or more equal to or lower than the Curie temperature.

14. (Currently Amended) A production method of crystal oriented ceramics comprising:

a mixing step in which an anisotropic shaped ~~power~~powder of plate-like crystal material, for which a crystal growth plane has lattice coherency with a specific crystal plane, is mixed with reaction material that can react therewith to form an isotropic perovskite compound of claim 1;

a molding step in which the mixture obtained in the mixing step is molded so that the specific anisotropic shaped powder crystal planes are oriented; and,

a heat treatment step in which the molded product obtained in the molding step is heated to cause a reaction between the anisotropic shaped powder and the reaction material to form a crystal oriented ceramic material as in claim 1.

15. (Previously Presented) A crystal oriented ceramics production method according to claim 14 wherein, the anisotropic shaped powder is a plate-like powder having the pseudo-cubic {100} plane for its growth plane and is represented by the following general formula:

$\{Li_x(K_{1-y}Na_y)_{1-x}\}\{Nb_{1-x-w}Ta_zSb_w\}O_3$

(wherein, x, y, z and w are $0 < x \leq 0.2$, $0 < y \leq 1$, $0 < z \leq 0.4$, $0 < w \leq 0.2$, respectively).

16. (Original) A piezoelectric element comprised of a piezoelectric material composed of crystal oriented ceramics according to claim 1.

17. (Original) A dielectric element comprised of a dielectric material composed of crystal oriented ceramics according to claim 1.

18-19. (Cancelled).